FORM PTO-1390 US DEPARTMENT OF COMMERCE REV. 5-99PATENT AND TRADEMARK OFFICE TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371		ATTORNEYS DOCKET NUMBER P01,0158
		U.S. APPLICATION NO. (If known, see 37 CFR 15)
INTERNATIONAL APPLICATION NO. PCT/DE99/03825	INTERNATIONAL FILING DATE 01 DECEMBER 1999	PRIORITY DATE CLAIMED 03 DECEMBER 1998
TITLE OF INVENTION METHOD AND ARRANGEMENT FOR DESIGNING A TECHNICAL SYSTEM		
APPLICANT(S) FOR DO/EO/US Stefan SCHÄFFLER et al.		
Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:		
This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 21 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 31 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 31 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 31 This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 31 This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 32 This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 32 This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 33 This is a FIRST submission of items concerning a filing under 35 U.S.C. 371. 34 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 35 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 36 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 37 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 38 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 39 This is a SECOND or SUBSEQUENT submission of items concerning a filing under 35 U.S.C. 371. 30 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 30 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 30 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 31 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 32 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 32 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 32 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 32 This is a SECOND or SUBSEQUENT submission of items concerning under 35 U.S.C. 371. 32		
\$\frac{\frac{1}{2}\text{id}}{\frac{1}{2}\text{id}}\$ A copy of International Application as filed (35 L.S.C. 371(c)(2)). \$\frac{1}{2}\text{id}\$ a \text{id}\$ is transmitted the herewith (recquited only! front transmitted by the International Bureau). \$\frac{1}{2}\text{id}\$ has been transmitted by the International Bureau. \$\frac{1}{2}\text{id}\$ is not required into was filed in the United States Receiving Office (RO/US) \$\frac{1}{2}\text{id}\$ A translation of the International Application into English (35 U.S.C. 371(c)(2).		
Amendments to the claims of the International Application under PCT Article 19 (35 U.S.C. §371(c)(3)) a		
A translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371(c)(3)).		
9. Man oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).		
10. a A translation of the ennexes to the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).		
Items 11. to 16. below concern other document(s) or information included: 11. An Information Disclosure Statement under 37 C.F.R. 1.97 and 1.98; (PTO 1449, Prior Art, Search Report, 10 References).		
12. b An assignment document for recording. A separate cover sheet in compliance with 37 C.F.R. 3.28 and 3.31 is included. (SEE ATTACHED ENVELOPE)		
13. Amendment "A" Prior to Action and Appendix "A". A SECOND or SUBSEQUENT preliminary amendment.		
14. A substitute specification and substitute specification mark-up.		
15. a A change of address letter attached to the Declaration.		
16. Other items or information: a. Submission of Orawings, 3 sheets of drawings, Figures 1-5 b. Appointment of Associate Power of Attorney c. EVPRESS MAIL, #EL 484728198 US dated June 1, 2001		

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BOX PCT IN THE UNITED STATES DESIGNATED/ELECTED OFFICE OF THE UNITED STATES PATENT AND TRADEMARK OFFICE UNDER THE PATENT COOPERATION TREATY--CHAPTER II

PRELIMINARY AMENDMENT A PRIOR TO ACTION

APPLICANT(S):

Stefan SCHÄFFLER et al.

ATTORNEY DOCKET NO .:

P01.0158

INTERNATIONAL APPLICATION NO: PCT/DE99/03825

INTERNATIONAL FILING DATE:

01 December 1999

INVENTION: METHOD AND ARRANGEMENT FOR DESIGNING A TECHNICAL SYSTEM

Assistant Commissioner for Patents,

Washington D.C. 20231

Sir:

Applicants herewith amend the above-referenced PCT application, and request entry of the Amendment prior to examination on the United States Examination Phase

IN THE CLAIMS:

On page 21:

replace line 1 with -- WHAT IS CLAIMED IS: --;

Please replace original claims 1-10 with the following rewritten claims 1-10. referring to the mark-ups in Appendix A.

- 1. (Amended) A method for designing a technical system, comprising the steps of:
 - a) providing a substitute model that describes measurement data of a predetermined system:
- b) determining a numerical value for a quality of said substitute model by comparing said measurement data of said predetermined system with data determined by said substitute model;

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of:

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- c) adapting said substitute model from said numerical value for said quality to be as high of a quality as possible;
- d) applying said substitute model adapted with regard to its quality in a design of said technical system.
- (Amended) The method as claimed in claim 1, wherein said substitute model is a regression model.
- (Amended) The method as claimed in claim 1, wherein said step of determining a numerical value for a quality further utilizes a mean square deviation of said measurement data from said data determined by said substitute model.
- 4. (Amended) The method as claimed in claim 1, further comprising the step of:

sorting said measurement data according to their quality, with respect to the deviation of the latter from said data determined by said substitute model; and picking out a predetermined number of n% of worst measurement data.

5. (Amended) The method as claimed in claim 1, further comprising the step

sorting said measurement data according to their quality, with respect to the deviation of the latter from said data determined by said substitute model; and picking out a predetermined number of n% of worst measurement data unless this data lie in a continuous range.

6. (Amended) The method as claimed in claim 1, further comprising the step of:

reducing an amount of measurement data in the course of a preprocessing operation.

7. (Amended) The method as claimed in claim 6, further comprising the step of:

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classifying, in which said preprocessing operation, of said measurement data.

8. (Amended) The method as claimed in claim 1, further comprising the step of:

controlling a technical plant utilizing said data obtained by designing.

9. (Amended) The method as claimed in claim 8, further comprising the step of:

online adapting control for said technical plant.

- (Amended) An arrangement for designing a technical system, comprising:
 - a processor unit which is set up in such a way that
- a) measurement data of a predetermined system are described based on a substitute model and stored in said processor unit;
- b) a numerical value for a quality of said substitute model is determined by said processor unit by comparing said measurement data of the predetermined system with data determined by said substitute model; and
- c) said substitute model is adapted, utilizing said processor unit, from said numerical value for said quality to be as of high a quality as possible, wherein said substitute model adapted with regard to its quality is used for designing said technical system.

REMARKS

The present Amendment revises the specification and claims to conform to United States patent practice, before examination of the present PCT application in the United States National Examination Phase. Pursuant to 37 CFR 1.125 (b), applicants have concurrently submitted a substitute specification, excluding the claims, and provided a marked-up copy. All of the changes are editorial and applicant believes no new matter is added thereby. The amendment, addition, and/or cancellation of claims is not intended to be a surrender of any of the subject matter of those claims.

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Early examination on the merits is respectfully requested.

Submitted by,

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Appendix A Mark Ups for Claim Amendments

This redlined draft, generated by CompareRite (TM) - The Instant Redliner, shows the differences between original document: Q:\DOCUMENTS\YEAR 2001\P010158-SCHAEFFLER-DESIGNING A TECHNICAL SYSTEMORIGINAL CLAIMS.DOC
and revised document: Q:\DOCUMENTS\YEAR 2001\P010158-SCHAEFFLER-DESIGNING A TECHNICAL SYSTEMOMENDED CLAIMS.DOC

10 CompareRite found 71 change(s) in the text

Deletions appear as Overstrike text surrounded by [] Additions appear as Bold-Underline text

- 1. (Amended) A method for designing a technical system, comprising the steps of:
- a) providing a substitute model that describes [a) in which] measurement data of a predetermined system [are described on the basis of a substitute model;];
- [b) in which] b) determining a numerical value for [the] a quality of [the] said substitute model [is determined] by comparing [the] said measurement data of [the] said predetermined system with data determined by [the] said substitute model;
- c) [in which the] adapting said substitute model [is adapted] from [the] said numerical value for [the] said quality to be [ef] as high of a quality as possible;
- d) [in which the] applying said substitute model adapted with regard to its quality [is used for designing the] in a design of said technical system.
- 2. (Amended) The method as claimed in claim 1, [in which the] wherein said substitute model is a regression model.
- 3. (Amended) The method as claimed in claim 1 [or 2, in which the], wherein said step of determining a numerical value for a quality [is-determined on the basis of] further utilizes a mean square deviation of [the] said measurement data from [the] said data determined by [the] said substitute model.
- 4. (Amended) The method as claimed in [ene of the preceding claims, in which the] claim 1, further comprising the step of:
- <u>sorting said</u> measurement data [are sorted] according to their quality, with respect to the deviation of the latter from [the] <u>said</u> data determined by [the] <u>said</u> substitute model[h]; and

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<u>picking out</u> a predetermined number of n% of [the] worst measurement data [are picked out].

(Amended) The method as claimed in claim [4, in which the n% of the]1.
 further comprising the step of:

sorting said measurement data according to their quality, with respect to the deviation of the latter from said data determined by said substitute model; and

picking out a predetermined number of n% of worst measurement data unless this data fare not-picked-out

if they lie in a continuous range.

6. (Amended) The method as claimed in [one-of the preceding claims, in which the] claim 1, further comprising the step of:

reducing an amount of measurement data [is-reduced] in the course of a preprocessing operation.

(Amended) The method as claimed in claim 6, fin which the -further comprising the step of:

classifying, in which said preprocessing operation [comprises-a classification of the], of said measurement data.

8. (Amended) The method as claimed in [one of the preceding claims, in which the] claim 1, further comprising the step of:

controlling a technical plant utilizing said data obtained by [means-of] designing [are used-for-controlling a technical plant.].

[9-]9. (Amended) The method as claimed in claim 8, [for] further comprising the step of:

online [adaptation of the] adapting control for [the] said technical plant.

- (<u>Amended</u>) An arrangement for designing a technical system, [with] <u>comprising:</u>
 - a processor unit which is set up in such a way that
- a) measurement data of a predetermined system are described <u>based</u> on [the basis of] a substitute model <u>and stored in said processor unit;</u>

- b) a numerical value for [the] <u>a</u> quality of [the] <u>said</u> substitute model is determined by <u>said processor unit by</u> comparing [the] <u>said</u> measurement data of the predetermined system with data determined by [the] <u>said</u> substitute model; <u>and</u>
- c) [the] said substitute model is adapted [from the], utilizing said processor unit, from said numerical value for [the] said quality to be as of [as] high a quality as possible, wherein said[;

the] substitute model adapted with regard to its quality is used for designing [the] said technical system.

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This redlined draft, generated by CompareRite (TM) - The Instant Redliner, shows the differences between - $\,$

original document : Q:\DOCUMENTS\YEAR 2001\P010158-SCHAEFFLER-DESIGNING A TECHNICAL SYSTEM\ORIGINAL SPECIFICATION.DOC

and revised document: Q:\DOCUMENTS\YEAR 2001\P010158-SCHAEFFLER-DESIGNING A TECHNICAL SYSTEM\SUBSTITUTE SPECIFICATION.DOC

CompareRite found 159 change(s) in the text

Deletions appear as Overstrike text surrounded by []
Additions appear as Bold-Underline text

SPECIFICATION

TITLE {DESCRIPTION}

METHOD AND ARRANGEMENT FOR DESIGNING A TECHNICAL SYSTEM

BACKGROUND OF THE INVENTION

Field of the Invention

[0001] The invention relates to a method and arrangement for designing a technical system.

Description of the Related Art

[0002] The system behavior of a technical system, for example, a process engineering plant or system in heavy industry, depends on numerous parameters. In the course of designing such a system, [that is in particular] particularly in the case of a new design or when adapting or adjusting an already existing system, it is necessary to comply with preconditions[, for example with regard to] such as the cost-effectiveness or environmental impact of the system. Each precondition is formulated as a target function, the loptimization of which with regard] general aim being to optimize this with respect to the other target functions [is the general aim.

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SUMMARY OF THE INVENTION

[0003] The object of the invention is to make it possible for a technical system to be designed on the basis of measurement data of a predetermined system. Specifically with regard to the optimization of the existing system or with regard to an optimized new design of a system, such use of known measurement data is of great significance.

[0004] This object is achieved faceording to the features of the independent patent claims. Developments of the invention also emerge from the dependent claims.

+a method and apparatus described below.

[0005] To achieve the object, the present invention provides a method for designing a technical system in which measurement data of a predetermined system are described on the basis of a substitute model [is specified]. A numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. [On the basis of] Based on the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible.

[0006] The substitute model adapted with regard to its quality is used for designing the technical system.

The measurement data obtained from many different realized systems are used for describing the substitute model. [With the] The substitute model [it is attempted] attempts to replicate the predetermined system as well as possible. numerical value for the quality of the replication is determined by comparing the actual measurement data with the data obtained on the basis of the substitute model. A great difference between the measurement data and the data of the substitute model corresponds to poor quality, that is, a poor mapping of the predetermined system into the substitute model. The numerical value for the quality is used to adapt the substitute model to make the quality itself become as high as possible and consequently to make the substitute model describe the predetermined system as well as possible. The high-quality substitute model obtained in this way is used for designing the technical system.

[0008] Designing is understood in a general sense as meaning both the new design of a technical system and the adaptation of an already existing technical system.

[0009] One development comprises that the substitute model is a regression model. The regression model is based on the description

[0010]
$$Y_i = f_6(x_i) + e_i$$

[0011] where

[0014] ei denotes an error.

$$\sum_{i=1}^{n} e_i^2 = \varphi(\beta).$$

[0016]

[0017] If the following example

[0018] $Y = \beta_0 + \beta_1 x + \beta_2 x^2 + e$

 $\begin{tabular}{ll} \hline \textbf{(0019)} & is taken as a basis, the functional relationship is of a quadratic order, while the regression model (function, dependent on <math>\beta$) is linear.

[0020] In another development, the quality can be determined on the basis of a mean square deviation of the measurement data from the data determined by the substitute model. The adaptation of the substitute model takes place by minimizing the mean square deviation.

One refinement comprises that the measurement data are [0021] sorted according to their quality, with respect to the deviation of the latter from the data determined by the substitute model, and a predetermined number of n% of the worst measurement data are picked out. Consequently, a quality is determined for each item of measurement data, the volume of measurement data, preferably in the form of a list, being sorted according to their quality and the n% of the worst measurement data, or the n worst measurement data, being picked out. In particular, it must be checked whether the n% of worst measurement data or n worst measurement data lie in a continuous range. If this is the case, these measurement data are not picked out, since they very probably do not represent measurement errors but a continuous range which is not mapped accurately enough by the substitute model.

[0022] Another development (comprises) that the (measure ment) measurement data are subjected to a preprocessing operation. Since, in an actual predetermined system, a large amount of measurement data occur per unit of time, it is advisable to subject these measurement data to a preprocessing operation and consequently ensure that largely significant measurement data are taken for forming the substitute model. The preprocessing operation preferably finds its expression in a reduction in the number of measurement data.

[0023] In the process, the measurement data are divided into classes according to predetermined criteria. The measured values of a class are assessed and those measured values for which the assessment lies below a predetermined first threshold value are picked out. The picking out of the measured values results in a reduction with regard to the number of measured values. This results in a significantly reduced number of measured values for a further processing

operation. The further processing operation can take place with less computing effort in comparison with the unreduced number of measured values.

[0024] The classes themselves can also be assessed. In particular, a class for which the assessment lies below a predetermined second threshold value can be picked out. As a result, an additional reduction of the number of measured values is obtained.

[0025] Another development of the preprocessing operation comprises that a criterion for the classification is that, for each class, measured values are determined as a default for setting parameters of the technical system. The technical system is typically set on the basis of a predetermined number of setting parameters; after setting, a reaction of the system to the setting parameters takes place (usually with a time delay) (transient response, transient phenomenon of the system). After setting, consequently a certain set of measured values which can be assigned to the transient phenomenon are recorded, with measured values continuing to occur after the transient phenomenon has come to an end (transition to steady-state operation), and are assigned to the predetermined set of setting parameters. [By adjusting] Adjusting the setting parameters [,] determines a new class [is $\frac{\text{determined}}{\text{determined}}$. All $\frac{\text{of}}{\text{the measured values which respectively}}$ occur after adjustment of the setting parameters belong in a class of their own.

[0026] In addition, measured values of a class which can be assigned to the respective transient phenomenon can be picked out. Furthermore, erroneous measured values can be picked out. The setting of large technical systems is in many cases directed at long-term steady-state operation. It is advisable for the measured values which relate to the transient phenomenon (of short duration in relation to the steady-state

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operation after the transient phenomenon has come to an end) to be picked out, since they have the effect of falsifying measured values for steady-state operation. In particular, when modeling the technical system, the measurement data of the steady-state behavior of the system are of interest.

[0027] One refinement comprises reducing the number of measured values in a class by determining at least one representative value for the measured values of the class. Such a representative value may be:

- a) a mean value (for example a sliding mean value) of the measured values of the class,
- b) a maximum value of the measured values of the class,
- c) a minimum value of the measured values of the class,
- d) a median.

[0028] In the case of variant d), one advantage is that a value which actually exists can always be determined, whereas the mean value a) does not itself occur as a value.

[0029] Depending on the application, a suitable choice can be made for determining the representative value of a class.

[0030] An entire class with measured values may be picked out if it contains less than a predetermined number of measured values.

[0031] Another refinement comprises that those measured values which vary by more than a predetermined threshold value from a predeterminable value are picked out. The predeterminable value may be a mean value of all the measured values of the class or a measured value to be expected in response to the respective setting parameters of the technical system.

[0032] Within another development, the data obtained by

[means] way of designing are used for controlling a technical
plant. In addition, the controlling of the technical plant
can take place at the running time of the system[, that is
enline.

+ (i.e., online).

10033] Also specified for achieving the object is an arrangement for designing a technical system which has a processor unit. Which processor unit is set up find such faway that measurement data of a predetermined system can be described on the basis of a substitute model. A numerical value for the quality of the substitute model can be determined by comparing the measurement data of the predetermined system with data determined by the substitute model. On the basis of the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible. The substitute model adapted with regard to its quality is used for designing the technical system.

[0034] This arrangement is particularly suitable for carrying out the method according to the invention or one of its developments explained above.

BRIEF DESCRIPTION OF THE DRAWINGS

[0035] Exemplary embodiments of the invention are presented and explained below with reference to the drawing, 4 lin which:

[ffigures 3-5-show input variables, manipulated variables and output] [0038] Figure 3 is a chart showing the input variables of the recovery boiler[...];

- 8 - MARK UP SUBSTITUTE SPECIFICATION

[Represented in figure 1 isl [0039] Figure 4 is a chart showing the manipulated variables of the recovery boiler; and

[0040] Figure 5 is a chart showing the output variables of the recovery boiler.

DETAILED DESCRIPTION OF THE INVENTION

[0041] Figure 1 shows a block diagram which contains steps of a method for designing a technical system. In a step 101, a substitute model (preferably a regression model) is formed on the basis of measurement data. [This substitute model is preferably a regression model.] To adapt the substitute model created in step 101 to the measurement data[, that is] (i.e., to perform a refinement of the substitute $model \frac{1}{1}$ so that the measurement data describe the substitute model in adequate approximation, a numerical value for the quality of the substitute model is determined in a step 102. This numerical value is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. Each item of measurement data preferably receives a numerical value for the quality, which numerical value characterizes the deviation of the item of measurement data from the associated value determined by the substitute model. The sum of all the numerical values for the quality for all the measurement data determines an overall quality for the substitute model. In a step 103, the quality is maximized by minimizing the numerical value for the quality (or a negative quality for the coincidence of the substitute model with the predetermined system). Once an appropriately high quality for the substitute model has been determined, this substitute model is used for designing the technical system in a step 104. The designing may constitute both a new design (cf. step 105) or an adaptation of an already existing technical system (cf. step 106).

[0042] Figure 2 shows a schematic diagram of a recovery boiler. An exemplary embodiment of the method described above is illustrated below on the basis of the example of a "recovery boiler".

[0043] In the paper and pulp industry, various chemicals and also heat and electrical energy are required for the digestion of pulp. The recovery boiler can be used to recover the chemicals used and also thermal energy from a concentrated process liquor (black liquor). [A] It is decisively significant to measure [ef] the recovery of the chemicals [is of decisive significance] for the cost-effectiveness of the overall plant.

10044] The black liquor is combusted in a char bed 201. As this happens, an alkali fusion is formed, flowing away via a line 202. In further process steps, the chemicals used are recovered from the constituents of the alkali fusion. Released heat of combustion is used for generating steam. The combustion of the waste liquor and consequently the recovery of the chemicals begins with the atomization of the black liquor via atomizer nozzles 204 into a combustion chamber 203. Particles of the atomized black liquor are dried as they fall through the hot flue gas. The dried liquor particles fall onto the char bed 201, with a first combustion and a chemical reduction taking place. Volatile constituents and reaction products pass into an exidation zone, in which exidizing reactions proceed and in which the combustion is completed.

[0045] Important targets for {the} controlling {of} the recovery boiler are the steam production for obtaining energy, the maintaining of emission values from environmental aspects and the efficiency of the chemical reduction.

[0046] The combustion operation, and consequently the targets, are controlled in particular by the air supply on three levels (Primary Air (PA), Secondary Air (SA), Tertiary Air (TA)). The overall process is subject to numerous influences, which have to be taken into account in the modeling:

- a) the measurement of the variables is often subject to strong fluctuations;
- b) unmeasured and unmeasurable influencing variables exist;
- any alteration of the parameters which can be set causes transient phenomena; and
- d) the technical plant becomes soiled and is cleaned at predetermined intervals, [having the result] resulting each time [of] in a temporal drift in the system behavior.

The measured variables of the overall process are [0047] divided into input variables (cf. [figure] Figure 3) and output variables (cf. $\{figure\}\ \underline{Figure}\ 5$). Measured values are stored every minute. Four of the input variables are at the same time also manipulated variables (also: parameters which can be set; cf. [figure] Figure 4). The manipulated variables are [to be] regarded essentially as free parameters of the overall process which can be set independently of one another. Some of the other input variables are more or less dependent on the manipulated variables. According to one target, in the case of the recovery boiler $\underline{\hspace{0.1in}}$ the "BL Front Pressure" and "BL Back Pressure" variables are always [to be] controlled such that they are the same. The four manipulated variables (cf. [figure] Figure 4) are preferably [to be] stored as manipulated variables (with the desired, preset value) and as input variables (with the measured, actual value).

[0048] In the case of the recovery boiler, one problem is

that of meeting targets which: 1) are determined in dependence on the parameters to be set, and 2) are defined by [means of] measured variables. A three-stage procedure is chosen here to solve the problem:

- 1. The targets to be considered are modeled by stochastic methods, these models being updated by new measurements (data-driven, empirical modeling). For this <u>step</u> it is advisable to use not just a single model but instead global models for the identification of areas of interest in a parameter space determined by the targets and local models for the exact calculation of optimum operating points. The models used are assessed by measures of quality.
- 2. If the models considered are not sufficiently accurate (measure of quality) for account off due to the data situation, new operating points are evaluated on a specific basis to improve the model (experimental design). Furthermore, by the use of global stochastic optimizing methods with respect to the targets, attractive areas are identified in dependence on the current global model.
- For the local optimization, local models are devised and, if appropriate, the available sets of data are extended on a specific basis (experimental design).

10049] The targets constitute physical-technical or business-management criteria, which generally have to conform to boundary conditions and/or safety conditions. Often a number of these criteria have to be considered simultaneously. The use of a stochastic model can be used in particular to simulate in the computer the target variables to be optimized and their dependence on the parameters to be set. This is necessary whenever measurements are very cost-intensive or very time-consuming. In the case of safety requirements, possible hazardous situations can be avoided.

[0050] In the case of the recovery boiler, an online optimization which is based on a number of data is necessary because the physical-chemical processes cannot be quantitatively modeled with sufficient accuracy and because the behavior of the plant is subject to fluctuations in the course of operation. Knowledge of this behavior must be continually extended by selective choice of new operating points. Therefore, the already described three-stage procedure of stochastic modeling and mathematical optimization is recommendable as part of online optimization.

DESCRIPTION OF THE INPUT VARIABLES

 $\begin{tabular}{ll} \hline \textbf{(0051)} & \textbf{The a input variables (a $\in N, N: set of natural numbers)} & \textbf{(and on random effects)} & \textbf{(b)} & \textbf{(b)} & \textbf{(c)} & \textbf{(c)}$

Borel σ algebra over \mathbb{O}^v (\mathbb{O} : set of real numbers) for each $v \in \mathbb{N}$. The input variables are represented by $\{means \ of \}$ a $B^n \times S - B^n$ -measurable mapping ϕ :

$$\phi: \mathbf{R}^{\mathbf{n}} \times \Omega \to \mathbf{R}^{\mathbf{a}} \tag{1}$$

 $\begin{tabular}{ll} \hline \textbf{(0053)} & The domain of the mapping ϕ is a Cartesian product of two sets. If the respective projections onto the individual sets are considered, the following mappings are obtained:$

[0054]

$$\phi_X : \Omega \to \mathbb{R}^a, \ \omega \to \phi(x, \omega) \quad \text{for all} \quad x \in \mathbb{R}^n$$
 (2),

[0055]

 $\varphi^{\omega} \colon \mathbf{R}^{n} \to \mathbf{R}^{a}, \ \mathbf{x} \to \varphi(\mathbf{x}, \omega) \quad \text{for all } \omega \in \Omega$ (3).

 $\frac{[0056]}{\left\{\phi_{X};\;\chi\;\in\;R^{n}\right\}}\quad \frac{[0057]}{\leftarrow}\quad \text{is a stochastic}$

 $\boxed{00591} \qquad \boxed{\mathbb{I}^n, \text{ and a mapping } \phi^\omega \text{ is, for each event } \omega \in \Omega, \text{ a}}$ path of this stochastic process.

[0060] In the case of the recovery boiler, n=4 and a=14 (after elimination of the "BL Back Pressure" variable).

 $\begin{tabular}{ll} \hline \textbf{On account of the required measurability of the} \\ \hline \textbf{mapping } \phi_X, & \text{for each } x \in \square^n \text{ the mapping } \phi_X \text{ is a random} \\ \hline \textbf{variable.} & \textbf{Under suitable additional preconditions,} \\ \hline \textbf{expectation values and higher moments can be considered. This approach permits the step from stochastic models to deterministic optimization problems. In the case of a deterministic optimization problem, the target function can be set directly by <math display="block"> \hline \textbf{[means of]} \text{ a variable, whereas the stochastic variable influences the target function but does not permit a specific setting.} \\ \hline \end{tabular}$

DESCRIPTION OF THE OUTPUT VARIABLES

 $\begin{tabular}{ll} \hline \begin{tabular}{ll} \hline \end{tabular} \\ \hline \end{tabular} \\ \hline \begin{tabular}{ll} \hline \end{tabular} \\ \hline \end{tabular} \\ \hline \begin{tabular}{ll} \hline \end{tabular} \\ \hline \end{t$

[0063]

$$M: \mathbf{R}^{\mathbf{a}} \times \Omega \to \mathbf{R}^{\mathbf{b}} \tag{4},$$

[0064] where b denotes the number of output variables.

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 $\begin{tabular}{ll} \hline \textbf{C0065]} & \textbf{Since the recovery boiler is subject to a cyclical temporal drift (from cleaning phase to cleaning phase), a description with a time parameter is also conceivable. The output variables can be represented by $B^n \times S - B^b$-measurable mappings ψ:} \\ \hline \end{tabular}$

[0066]

$$\Psi: \mathbf{R}^{\mathbf{n}} \times \Omega \to \mathbf{R}^{\mathbf{b}} \tag{5},$$

$$(x, \omega) \to M(\varphi(x, \omega), \omega)$$
 (6)

[0067] If the respective projections onto the individual sets of the domain are considered, the following mappings are obtained

[0068]

$$\psi_{\mathbf{X}}: \Omega \to \mathbf{R}^{\mathbf{b}}, \ \omega \to \psi(\mathbf{x}, \omega) \quad \text{for all} \quad \mathbf{x} \in \mathbf{R}^{\mathbf{n}}$$
 (7),

$$\psi^{\omega} \colon \mathbb{R}^{n} \to \mathbb{R}^{b}, \ x \to \psi(x, \omega) \quad \text{for all} \quad \omega \in \Omega$$
(8).

[0069] is a stochastic process with an index set

$$\{\psi_{\mathbf{X}}; \mathbf{x} \in \mathbf{R}^{n}\}$$

 $\boxed{00721} \qquad \square^n, \text{ and the mapping } \psi^\omega \text{ is, for each } \omega \in \Omega, \text{ a path of this stochastic process.}$

[0073] In the case of the recovery boiler, b=15.

 $\begin{tabular}{ll} \hline \textbf{(0074)} & \textbf{The fact that in the definition of ψ a distinction} \\ \hline \textbf{is not drawn between the events ω used does not mean that} \\ \hline \textbf{there is any restriction, since Ω can be represented as a} \\ \hline \end{tabular}$

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Cartesian product of an Ω_1 and an Ω_2 . The above representation consequently also comprises the model:

[0075]

$$\Psi: \mathbf{R}^{\mathbf{n}} \times \Omega_{1} \times \Omega_{2} \to \mathbf{R}^{\mathbf{b}} \tag{9},$$

$$(x, \omega_1, \omega_2) \rightarrow M(\varphi(x, \omega_1), \omega_2)$$
 (10).

DESCRIPTION OF THE AVAILABLE SETS OF DATA

 $\begin{tabular}{ll} \hline \textbf{(0076]} & \begin{tabular}{ll} \textbf{With the descriptions in the two foregoing sections,} \\ \hline \textbf{the input variables and the output variables can be combined} \\ \hline \textbf{together to form measured variables (= measurement data)} & \begin{tabular}{ll} \Phi. & \begin{tabular}{ll} \Phi \\ \hline \textbf{is a } B^n \times S - B^m\text{-measurable mapping with } m = a + b \ and \\ \hline \end{tabular}$

[0077]

$$\Phi: \mathbf{R}^{n} \times \Omega \to \mathbf{R}^{m} \tag{11},$$

$$(x, \omega) \rightarrow \begin{pmatrix} \phi(x, \omega) \\ \psi(x, \omega) \end{pmatrix}$$
 (12).

[0078] If the respective projections onto the individual sets of the domain are again considered, the following mappings are obtained:

$$\Phi_X \colon \Omega \, \to \, R^m, \; \omega \, \to \, \Phi(x, \, \omega) \quad \text{ for all } \qquad \quad x \, \in \, R^n \tag{13} \, ,$$

$$\Phi^{\omega} \colon \mathbb{R}^{n} \to \mathbb{R}^{m}, \ x \to \Phi(x, \omega) \quad \text{for all} \qquad \omega \in \Omega$$
 (14).

[0079] [0080] is a stochastic process with an index set

$$\{\Phi_{\mathbf{X}}; \mathbf{x} \in \mathbf{R}^n\}$$

 $\boxed{0082]} \qquad \boxed{\mathbb{D}^n}, \text{ and the mapping } \Phi^\omega \text{ is, for each } \omega \in \Omega, \text{ a path of this stochastic process.}$

 $\begin{tabular}{ll} \hline \mbox{ For each chosen related variable tupel x, in the case of the recovery boiler many realizations of Φ_x are determined and stored, i.e., for each $x_j \in {\Bbb P}^n$ numerous realizations$

[0084]

$$\Phi_{j\,k} := \Phi(x_j, \omega_{j\,k})$$
with $\omega_{j\,k} \in \Omega$; $k = 1, 2, ..., v_j$;
$$v_j \in N$$
; $j = 1, 2, ..., u$; $u \in N$

 $\begin{tabular}{ll} \hline \textbf{(0085)} & are considered. & The stored sets of data D_{jk} of the recovery boiler are consequently $(n+m)$ tupels: $$ \end{tabular}$

[0086]

$$D_{jk} = \begin{pmatrix} x_j \\ \Phi_{jk} \end{pmatrix}, \qquad k = 1, 2, \dots, v_j; \quad j = 1, 2, \dots, u \tag{16} \label{eq:16} \ .$$

[0089] applies.

DATA COMPRESSION BY CLASSIFICATION OF THE PARAMETERS [0090] Since for each manipulated variable tupel x there

are generally a number of realizations of Φ_x , a classification of the parameters by forming arithmetic mean values is a suitable operation as a first step of the statistical data analysis on account of the complex stochastic properties of the process to be considered. Moreover, sets of data which are obviously erroneous are picked out. A set of data which is obviously erroneous is, for example, a physically impossible measurement which cannot occur in reality, fin particular on account off particularly due to a setting made.

[0091] Procedure:

- Sets of data in which the "BL Front Pressure" variable is not equal to the "BL Back Pressure" variable are picked out, since these two values must be equal according to the default of the plant control. The data loss is very small.
- The sets of data are divided into classes in which the four setting parameters (PA, SA, TA, BL Front Pressure, see above) are constant in temporal succession,

[0092] i.e., the jth class comprises the data sets D_i.

- Classes in which there are fewer than 30 data sets are picked out in order that transient phenomena have no great influence.
- 4. For each class, an arithmetic mean value Φ_j —and an empirical standard deviation s_j are determined for all the measured variables:

[0093]

$$\overline{\Phi}_{j} = \frac{1}{v_{j}} \cdot \sum_{k=1}^{v_{j}} \Phi_{jk} \tag{17},$$

$$s_{j} = \begin{pmatrix} \left(\frac{1}{v_{j}-1} \cdot \sum_{k=1}^{v_{j}} \left(\Phi_{jk}^{(l)} - \overline{\Phi}_{j}^{(l)}\right)^{2}\right)^{\frac{1}{2}} \\ \vdots \\ \left(\frac{1}{v_{j}-1} \cdot \sum_{k=1}^{v_{j}} \left(\Phi_{jk}^{(m)} - \overline{\Phi}_{j}^{(m)}\right)^{2}\right)^{\frac{1}{2}} \end{pmatrix}$$
(18).

5. Classes in which the mean values for the variables PA, SA, TA or BL Front Pressure are too far away from the corresponding setting parameters are picked out. Therefore, in these classes it {was} is not possible to reach the setting values.

STATISTICAL CHARACTERISTIC VARIABLES FOR THE GIVEN CLASSES AND THEIR GRAPHIC REPRESENTATION

[0094] Apart from the arithmetic mean values and the empirical standard deviations which were determined for the individual classes, a common standard deviation s is also determined according to

[0095]

$$\mathbf{s} = \begin{pmatrix} \left(\frac{1}{v-1} \cdot \sum_{j=1}^{u} (v_{j} - 1) \mathbf{s}_{j}^{(1)2}\right)^{\frac{1}{2}} \\ \vdots \\ \left(\frac{1}{v-1} \cdot \sum_{j=1}^{u} (v_{j} - 1) \mathbf{s}_{j}^{(m)2}\right)^{\frac{1}{2}} \end{pmatrix}$$
(19)

[0096] where u stands for the number of classes (here 205) and v stands for the sum of v_j , i.e., v is the number of all the measured values used (here 38915).

LINEAR REGRESSION MODELS FOR FUNCTION APPROXIMATIONS

 $\label{eq:problem} \begin{array}{ll} \hbox{ \cite{thm of measurement measured variable (item of measurement)}} \\ \hbox{ \cite{thm of measurement)}} \\$

[0098] x⁽¹⁾: Primary Air (PA)

[0099] $x^{(2)}$: Secondary Air (SA)

 $x^{(3)}$: Tertiary Air (TA)

[00101] $x^{(4)}$: Black Liquor (BL) Front Pressure

 $\begin{tabular}{ll} \hline (00102] & applies. & u \in N \end{tabular} \label{eq:continuous} \ \ denotes the number of classes. Each measured variable <math display="inline">\Phi^{(i)}$ is modeled by

[00103]

$$\Phi^{(i)}(x,\omega) = a_i^T r(x) + e_i(\omega)$$
 (20)

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$$r: \mathbf{R}^4 \to \mathbf{R}^{15} \tag{21}$$

[00106] i.e., polynomials of the second degree are adapted to the measurement data, and

[00107]

$$e_{\dot{1}}:\Omega\to R$$
 (23)

[00108] is a random variable with the expected value 0.

[00109] The vector ai is determined by the method of

[00110] least squares, but the [-][00111]

arithmetic means

$$\left(x_{j}, \Phi_{jk}^{(i)}\right)^{T}$$

[00113] are used instead of the original data sets

$$\left(x_{j}, \overline{\Phi}_{j}^{(i)}\right)^{T}$$

[00116] This procedure is suitable, since linear regression models estimate in particular expected values. This results in the following minimization problem:

[00117]

$$\min_{\mathbf{a}_{\underline{i}} \in \mathbf{R}^{15}} \left\{ \left\| \begin{pmatrix} \overline{\Phi}_{\underline{i}}^{(i)} \\ \vdots \\ \overline{\Phi}_{\underline{i}}^{(i)} \end{pmatrix} - \begin{pmatrix} \mathbf{r}(\mathbf{x}_{\underline{1}})^{\mathrm{T}} \\ \vdots \\ \mathbf{r}(\mathbf{x}_{\underline{u}})^{\mathrm{T}} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{a}_{\underline{i}}^{(1)} \\ \vdots \\ \mathbf{a}_{\underline{i}}^{(15)} \end{pmatrix} \right\|_{2}^{2} \right\}$$
(24).

[00119]

$$\hat{y}_{\underline{i}} := \begin{pmatrix} r(x_{\underline{1}})^{T} \\ \vdots \\ r(x_{\underline{u}})^{T} \end{pmatrix} \cdot \begin{pmatrix} \overline{a}_{\underline{i}}^{(1)} \\ \vdots \\ \overline{a}_{\underline{i}}^{(15)} \end{pmatrix} \in \mathbf{R}^{\underline{u}}$$
(25),

$$\overline{y}_{i} := \frac{1}{u} \cdot \sum_{j=1}^{u} \overline{\Phi}_{j}^{(i)} \in \mathbf{R}$$
 (26).

 $\underline{\hbox{[00120]}} \qquad \hbox{To validate the regression theorem, a coefficient of determination R^2 is calculated according to $$[with]$$

<u>-[00121]</u>

$$\mathbb{R}^{2} := \frac{\sum_{j=1}^{u} \left(\hat{y}_{1}^{(j)} - \overline{y}_{1}\right)^{2}}{\sum_{i=1}^{u} \left(\overline{\Phi}_{1}^{(i)} - \overline{y}_{1}\right)^{2}} = \frac{\hat{y}_{1}^{T} \hat{y}_{1} - u \overline{y}_{1}^{2}}{\overline{\Phi}^{(1)T} \overline{\Phi}^{(1)} - u \overline{y}_{1}^{2}}$$
(27)

[00122] with

[00123]

$$\overline{\Phi}^{(i)} = \begin{pmatrix} \overline{\Phi}_{1}^{(i)} \\ \vdots \\ \overline{\Phi}_{u}^{(i)} \end{pmatrix} \tag{28}$$

[00124] The closer R_i^2 is to 1, the better the dependent variable is represented by the independent variables $\{0 \le R_1^2 \le 1\}$

 ${\hbox{\hbox{$\tt [00125]}}}$ In addition, a maximum ${\hbox{$\tt E$}^{(i)}}_{max}$ for an absolute value of the deviation of the data from the model is specified as ${\hbox{\hbox{$\tt [00126]}}}$

$$E_{\text{max}}^{(i)} := \max_{j=1,\dots,u} \left\{ \left| \overline{\Phi}_{j}^{(i)} - \hat{y}_{1}^{(j)} \right| \right\}$$
 (29).

 $\begin{array}{ll} \underline{\textbf{1001271}} & E^{(4)}_{90\$} \text{ is that value below which at least 90\$ of the absolute values of the deviations of the data from the model lie. By analogy with this, <math>E^{(4)}_{80\$}$ is that value below which at least 80\\$ of the absolute values of the deviations of the data from the model lie. With the optimum point a_i of the minimization problem according to equation (24), a model $\tilde{\Phi}^{(i)}$ of the expected value of the measured variable $\Phi^{(4)}$ can be specified as

[00128]

$$\tilde{\Phi}^{(i)} := \mathbb{R}^{n} \to \mathbb{R} \tag{30},$$

$$x \to \overline{a}_i^T r(x)$$
 (31).

[00129] In particular, the gradient $\nabla \tilde{\Phi}^{(i)}$ and analytically specified by

[00130]

$$\nabla \widetilde{\Phi}^{(\underline{i})}(x) = \frac{dr}{dx}(x) \cdot \overline{a}_{\underline{i}} \quad \text{for all} \quad x \in \mathbf{R}^{\Pi}$$
 (32).

[00131] The above-described method and system are illustrative of the principles of the present invention.

Numerous modifications and adaptations will be readily apparent to those skilled in this art without departing from the spirit and scope of the present invention.

ABSTRACT

[Method and arrangement for designing a technical system

To achieve the object, a method | [00132] A method is provided for designing a technical system in which measurement data of a predetermined system are described based on [the basis of] a substitute model [is specified]. A numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. On the basis of the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible. The substitute model adapted with regard to its quality is used for designing the technical system.

SPECIFICATION

TITLE

METHOD AND ARRANGEMENT FOR DESIGNING A TECHNICAL SYSTEM

BACKGROUND OF THE INVENTION

Field of the Invention

[0001] The invention relates to a method and arrangement for designing a technical system.

Description of the Related Art

[0002] The system behavior of a technical system, for example, a process engineering plant or system in heavy industry, depends on numerous parameters. In the course of designing such a system, particularly in the case of a new design or when adapting or adjusting an already existing system, it is necessary to comply with preconditions such as the cost-effectiveness or environmental impact of the system. Each precondition is formulated as a target function, the general aim being to optimize this with respect to the other target functions.

SUMMARY OF THE INVENTION

[0003] The object of the invention is to make it possible for a technical system to be designed on the basis of measurement data of a predetermined system. Specifically with regard to the optimization of the existing system or with regard to an optimized new design of a system, such use of known measurement data is of great significance.

[0004] This object is achieved a method and apparatus described below.

[0005] To achieve the object, the present invention provides a method for designing a technical system in which measurement data of a predetermined system are described on

the basis of a substitute model. A numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. Based on the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible.

[0006] The substitute model adapted with regard to its quality is used for designing the technical system.

The measurement data obtained from many different realized systems are used for describing the substitute model. The substitute model attempts to replicate the predetermined system as well as possible. The numerical value for the quality of the replication is determined by comparing the actual measurement data with the data obtained on the basis of the substitute model. A great difference between the measurement data and the data of the substitute model corresponds to poor quality, that is, a poor mapping of the predetermined system into the substitute model. The numerical value for the quality is used to adapt the substitute model to make the quality itself become as high as possible and consequently to make the substitute model describe the predetermined system as well as possible. The high-quality substitute model obtained in this way is used for designing the technical system.

[0008] Designing is understood in a general sense as meaning both the new design of a technical system and the adaptation of an already existing technical system.

[0009] One development comprises that the substitute model is a regression model. The regression model is based on the description

[0010]
$$Y_i = f_R(x_i) + e_i$$

[0011] where

[0012] (y_i, x_i) denotes predetermined pairs of

values,

[0013] $f_{\beta_{\parallel}}$ denotes a function which is dependent on a parameter β_{ν} and

[0014] e denotes an error.

[0015] It is then intended to minimize the error (as a function of β):

$$\sum_{i=1}^{n} e_i^2 = \varphi(\beta).$$

[0016]

[0017] If the following example

[0018]
$$Y = \beta_0 + \beta_1 x + \beta_2 x^2 + e$$

[0019] is taken as a basis, the functional relationship is of a quadratic order, while the regression model (function, dependent on β) is linear.

[0020] In another development, the quality can be determined on the basis of a mean square deviation of the measurement data from the data determined by the substitute model. The adaptation of the substitute model takes place by minimizing the mean square deviation.

[0021] One refinement comprises that the measurement data are sorted according to their quality, with respect to the deviation of the latter from the data determined by the substitute model, and a predetermined number of n% of the worst measurement data are picked out. Consequently, a quality is determined for each item of measurement data, the volume of measurement data, preferably in the form of a list, being sorted according to their quality and the n% of the worst measurement data, or the n worst measurement data, being picked out. In particular, it must be checked whether the n% of worst measurement data or n worst measurement data lie in a continuous range. If this is the case, these measurement data are not picked out, since they very

probably do not represent measurement errors but a continuous range which is not mapped accurately enough by the substitute model.

[0022] Another development comprises that the measurement data are subjected to a preprocessing operation. Since, in an actual predetermined system, a large amount of measurement data occur per unit of time, it is advisable to subject these measurement data to a preprocessing operation and consequently ensure that largely significant measurement data are taken for forming the substitute model. The preprocessing operation preferably finds its expression in a reduction in the number of measurement data.

[0023] In the process, the measurement data are divided into classes according to predetermined criteria. The measured values of a class are assessed and those measured values for which the assessment lies below a predetermined first threshold value are picked out. The picking out of the measured values results in a reduction with regard to the number of measured values. This results in a significantly reduced number of measured values for a further processing operation. The further processing operation can take place with less computing effort in comparison with the unreduced number of measured values.

[0024] The classes themselves can also be assessed. In particular, a class for which the assessment lies below a predetermined second threshold value can be picked out. As a result, an additional reduction of the number of measured values is obtained.

[0025] Another development of the preprocessing operation comprises that a criterion for the classification is that, for each class, measured values are determined as a default for setting parameters of the technical system. The technical system is typically set on the basis of a predetermined number of setting parameters; after setting, a reaction of the system

to the setting parameters takes place (usually with a time delay) (transient response, transient phenomenon of the system). After setting, consequently a certain set of measured values which can be assigned to the transient phenomenon are recorded, with measured values continuing to occur after the transient phenomenon has come to an end (transition to steady-state operation), and are assigned to the predetermined set of setting parameters. Adjusting the setting parameters determines a new class. All of the measured values which respectively occur after adjustment of the setting parameters belong in a class of their own.

[0026] In addition, measured values of a class which can be assigned to the respective transient phenomenon can be picked out. Furthermore, erroneous measured values can be picked out. The setting of large technical systems is in many cases directed at long-term steady-state operation. It is advisable for the measured values which relate to the transient phenomenon (of short duration in relation to the steady-state operation after the transient phenomenon has come to an end) to be picked out, since they have the effect of falsifying measured values for steady-state operation. In particular, when modeling the technical system, the measurement data of the steady-state behavior of the system are of interest.

[0027] One refinement comprises reducing the number of measured values in a class by determining at least one representative value for the measured values of the class. Such a representative value may be:

- a) a mean value (for example a sliding mean value) of the measured values of the class.
- b) a maximum value of the measured values of the class.
- c) a minimum value of the measured values of the class,
- d) a median.
- [0028] In the case of variant d), one advantage is that a

value which actually exists can always be determined, whereas the mean value a) does not itself occur as a value.

[0029] Depending on the application, a suitable choice can be made for determining the representative value of a class.

[0030] An entire class with measured values may be picked out if it contains less than a predetermined number of measured values.

[0031] Another refinement comprises that those measured values which vary by more than a predetermined threshold value from a predeterminable value are picked out. The predeterminable value may be a mean value of all the measured values of the class or a measured value to be expected in response to the respective setting parameters of the technical system.

[0032] Within another development, the data obtained by way of designing are used for controlling a technical plant. In addition, the controlling of the technical plant can take place at the running time of the system (i.e., online).

[0033] Also specified for achieving the object is an arrangement for designing a technical system which has a processor unit set up such that measurement data of a predetermined system can be described on the basis of a substitute model. A numerical value for the quality of the substitute model can be determined by comparing the measurement data of the predetermined system with data determined by the substitute model. On the basis of the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible. The substitute model adapted with regard to its quality is used for designing the technical system.

[0034] This arrangement is particularly suitable for carrying out the method according to the invention or one of its developments explained above.

BRIEF DESCRIPTION OF THE DRAWINGS

[0035] Exemplary embodiments of the invention are presented and explained below with reference to the drawing, in which:

[0036] Figure 1 is a block diagram which contains steps of a method for designing a technical system;

[0037] Figure 2 is a schematic diagram of a recovery boiler;

[0038] Figure 3 is a chart showing the input variables of the recovery boiler;

[0039] Figure 4 is a chart showing the manipulated variables of the recovery boiler; and

[0040] Figure 5 is a chart showing the output variables of the recovery boiler.

DETAILED DESCRIPTION OF THE INVENTION

Figure 1 shows a block diagram which contains steps of a method for designing a technical system. In a step 101, a substitute model (preferably a regression model) is formed on the basis of measurement data. To adapt the substitute model created in step 101 to the measurement data (i.e., to perform a refinement of the substitute model) so that the measurement data describe the substitute model in adequate approximation, a numerical value for the quality of the substitute model is determined in a step 102. This numerical value is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. Each item of measurement data preferably receives a numerical value for the quality, which numerical value characterizes the deviation of the item of measurement data from the associated value determined by the substitute model. The sum of all the numerical values for the quality for all the measurement data determines an overall quality for the substitute model. In a step 103, the quality is maximized by minimizing the numerical value for the quality (or a negative - 7 -SUBSTITUTE SPECIFICATION quality for the coincidence of the substitute model with the predetermined system). Once an appropriately high quality for the substitute model has been determined, this substitute model is used for designing the technical system in a step 104. The designing may constitute both a new design (cf. step 105) or an adaptation of an already existing technical system (cf. step 106).

[0042] Figure 2 shows a schematic diagram of a recovery boiler. An exemplary embodiment of the method described above is illustrated below on the basis of the example of a "recovery boiler".

[0043] In the paper and pulp industry, various chemicals and also heat and electrical energy are required for the digestion of pulp. The recovery boiler can be used to recover the chemicals used and also thermal energy from a concentrated process liquor (black liquor). It is decisively significant to measure the recovery of the chemicals for the costeffectiveness of the overall plant.

[0044] The black liquor is combusted in a char bed 201. As this happens, an alkali fusion is formed, flowing away via a line 202. In further process steps, the chemicals used are recovered from the constituents of the alkali fusion. Released heat of combustion is used for generating steam. The combustion of the waste liquor and consequently the recovery of the chemicals begins with the atomization of the black liquor via atomizer nozzles 204 into a combustion chamber 203. Particles of the atomized black liquor are dried as they fall through the hot flue gas. The dried liquor particles fall onto the char bed 201, with a first combustion and a chemical reduction taking place. Volatile constituents and reaction products pass into an oxidation zone, in which oxidizing reactions proceed and in which the combustion is completed.

[0045] Important targets for controlling the recovery boiler are the steam production for obtaining energy, the

maintaining of emission values from environmental aspects and the efficiency of the chemical reduction.

[0046] The combustion operation, and consequently the targets, are controlled in particular by the air supply on three levels (Primary Air (PA), Secondary Air (SA), Tertiary Air (TA)). The overall process is subject to numerous influences, which have to be taken into account in the modeling:

- a) the measurement of the variables is often subject to strong fluctuations;
- b) unmeasured and unmeasurable influencing variables exist;
- any alteration of the parameters which can be set causes transient phenomena; and
- d) the technical plant becomes soiled and is cleaned at predetermined intervals, resulting each time in a temporal drift in the system behavior.

The measured variables of the overall process are divided into input variables (cf. Figure 3) and output variables (cf. Figure 5). Measured values are stored every minute. Four of the input variables are at the same time also manipulated variables (also: parameters which can be set; cf. Figure 4). The manipulated variables are regarded essentially as free parameters of the overall process which can be set independently of one another. Some of the other input variables are more or less dependent on the manipulated variables. According to one target, in the case of the recovery boiler, the "BL Front Pressure" and "BL Back Pressure" variables are always controlled such that they are the same. The four manipulated variables (cf. Figure 4) are preferably stored as manipulated variables (with the desired, preset value) and as input variables (with the measured, actual value).

[0048] In the case of the recovery boiler, one problem is that of meeting targets which: 1) are determined in dependence on the parameters to be set, and 2) are defined by measured variables. A three-stage procedure is chosen here to solve the problem:

- 1. The targets to be considered are modeled by stochastic methods, these models being updated by new measurements (data-driven, empirical modeling). For this step it is advisable to use not just a single model but instead global models for the identification of areas of interest in a parameter space determined by the targets and local models for the exact calculation of optimum operating points. The models used are assessed by measures of quality.
- 2. If the models considered are not sufficiently accurate (measure of quality) due to the data situation, new operating points are evaluated on a specific basis to improve the model (experimental design). Furthermore, by the use of global stochastic optimizing methods with respect to the targets, attractive areas are identified in dependence on the current global model.
- For the local optimization, local models are devised and, if appropriate, the available sets of data are extended on a specific basis (experimental design).

[0049] The targets constitute physical-technical or business-management criteria, which generally have to conform to boundary conditions and/or safety conditions. Often a number of these criteria have to be considered simultaneously. The use of a stochastic model can be used in particular to simulate in the computer the target variables to be optimized and their dependence on the parameters to be set. This is necessary whenever measurements are very cost-intensive or very time-consuming. In the case of safety requirements, possible hazardous situations can be avoided.

[0050] In the case of the recovery boiler, an online

optimization which is based on a number of data is necessary because the physical-chemical processes cannot be quantitatively modeled with sufficient accuracy and because the behavior of the plant is subject to fluctuations in the course of operation. Knowledge of this behavior must be continually extended by selective choice of new operating points. Therefore, the already described three-stage procedure of stochastic modeling and mathematical optimization is recommendable as part of online optimization.

DESCRIPTION OF THE INPUT VARIABLES

[0051] The a input variables (a \in N, N: set of natural numbers) are generally dependent on n actuated variables n \in N and on random effects. They can be described as follows:

[0052] Let (Ω, S, P) be a probability space and B^v be a Borel σ algebra over \mathbb{D}^v (\mathbb{D} : set of real numbers) for each $v \in N$. The input variables are represented by a $B^n \times S - B^a$ -measurable mapping ϕ :

$$\varphi: \mathbf{R}^{n} \times \Omega \to \mathbf{R}^{a} \tag{1}$$

[0053] The domain of the mapping ϕ is a Cartesian product of two sets. If the respective projections onto the individual sets are considered, the following mappings are obtained:

$$\phi_{\mathbf{X}}: \Omega \to \mathbb{R}^{\mathbf{a}}, \ \omega \to \phi(\mathbf{x}, \omega) \quad \text{for all} \qquad \mathbf{x} \in \mathbb{R}^{\mathbf{n}} \tag{2},$$

 $\varphi^{\omega} \colon \mathbb{R}^{n} \to \mathbb{R}^{a}, \ x \to \varphi(x, \omega) \quad \text{for all } \omega \in \Omega$ (3).

[0055]
$$\phi^{-1}: \mathbf{K}^{-1} \to \mathbf{K}^{-1}, \ \mathbf{x} \to \phi(\mathbf{x}, \omega) \quad \text{for all } \ \omega \in \Omega$$

 $\left\{ \begin{matrix} \phi_{\mathbf{x}}, \ \mathbf{x} \in \mathbf{f} \\ \end{matrix} \right. \text{ with an index set}$

[0058] $\hfill\Box^n,$ and a mapping ϕ^ω is, for each event $\omega\in\Omega,$ a path of this stochastic process.

[0059] In the case of the recovery boiler, n=4 and a=14 (after elimination of the "BL Back Pressure" variable).

[0060] On account of the required measurability of the mapping ϕ_x , for each $x \in \mathbb{I}^n$ the mapping ϕ_x is a random variable. Under suitable additional preconditions, expectation values and higher moments can be considered. This approach permits the step from stochastic models to deterministic optimization problems. In the case of a deterministic optimization problem, the target function can be set directly by a variable, whereas the stochastic variable influences the target function but does not permit a specific setting.

DESCRIPTION OF THE OUTPUT VARIABLES

[0061] The process model M of the recovery boiler is described as a function in dependence on the input variables and further random effects. In this case let $(\Omega, 5, P)$ be the above probability space. The process model M is then a $B^a \times S - B^b$ -measurable mapping:

$$M: \mathbb{R}^{a} \times \Omega \to \mathbb{R}^{b} \tag{4},$$

[0062]

[0063] where b denotes the number of output variables.

[0064] Since the recovery boiler is subject to a cyclical temporal drift (from cleaning phase to cleaning phase), a description with a time parameter is also conceivable. The output variables can be represented by $B^n\times S$ - B^b -measurable mappings $\psi\colon$

$$\Psi: \mathbf{R}^{n} \times \mathbf{\Omega} \to \mathbf{R}^{b} \tag{5},$$

$$(x, \omega) \rightarrow M(\varphi(x, \omega), \omega)$$
 (6).

[0066] If the respective projections onto the individual sets of the domain are considered, the following mappings are - 12 - Substitute Specification

$$\psi_{\mathbf{x}} \colon \Omega \to \mathbf{R}^{\mathsf{b}}, \ \omega \to \psi(\mathbf{x}, \omega) \quad \text{for all} \quad \mathbf{x} \in \mathbf{R}^{\mathsf{n}}$$
 (7),

$$\psi^{\omega} \colon R^{n} \to R^{b}, \ x \to \psi(x, \omega) \quad \text{for all} \quad \omega \in \Omega \tag{8} \ .$$

[0068]

 $\{ \psi_{\mathbf{X}}; \ \mathbf{x} \in \text{with an index set}$

[0070] $\ \Box^n,$ and the mapping ψ^ω is, for each $\omega\in\Omega,$ a path of this stochastic process.

[0071] In the case of the recovery boiler, b=15.

[0072] The fact that in the definition of ψ a distinction is not drawn between the events ω used does not mean that there is any restriction, since Ω can be represented as a Cartesian product of an Ω_1 and an Ω_2 . The above representation consequently also comprises the model:

$$\psi: \mathbf{R}^{\mathbf{n}} \times \Omega_1 \times \Omega_2 \to \mathbf{R}^{\mathbf{b}} \tag{9}$$

$$(x, \omega_1, \omega_2) \rightarrow M(\varphi(x, \omega_1), \omega_2)$$
 (10).

[0073]

DESCRIPTION OF THE AVAILABLE SETS OF DATA

[0074] With the descriptions in the two foregoing sections, the input variables and the output variables can be combined together to form measured variables (= measurement data) Φ . Φ is a $B^n \times S$ - B^n -measurable mapping with m = a + b and

$$\Phi: \mathbf{R}^{n} \times \Omega \to \mathbf{R}^{m} \tag{11},$$

$$(\mathbf{x}, \boldsymbol{\omega}) \to \begin{pmatrix} \varphi(\mathbf{x}, \boldsymbol{\omega}) \\ \psi(\mathbf{x}, \boldsymbol{\omega}) \end{pmatrix}$$
 (12).

[0075]

[0076] If the respective projections onto the individual

sets of the domain are again considered, the following mappings are obtained:

$$\Phi_X \colon \Omega \, \to \, \boldsymbol{R}^m, \; \omega \, \to \, \Phi(x,\omega) \quad \text{ for all } \qquad x \, \in \, \boldsymbol{R}^n \tag{13)} \, ,$$

$$\Phi^{\omega} \colon \mathbb{R}^{n} \to \mathbb{R}^{m}, \ x \to \Phi(x, \omega) \quad \text{for all} \quad \omega \in \Omega$$
 (14).

 $\left\{ \Phi_{X}; \; x \; \in \begin{bmatrix} 0078 \end{bmatrix} \quad \text{is a stochastic process} \\ \text{with an index set} \right.$

[0079] $\ \Box^n,$ and the mapping Φ^ω is, for each $\omega\in\Omega,$ a path of this stochastic process.

[0080] For each chosen related variable tupel x, in the case of the recovery boiler many realizations of Φ_x are determined and stored, i.e., for each $x_j \in \mathbb{D}^n$ numerous realizations

$$\Phi_{jk} := \Phi(x_j, \omega_{jk}) \tag{15}$$

with
$$\omega_{jk} \in \Omega$$
; $k = 1,2,...,v_j$;

 $v_j \in N$; j = 1,2,...,u; $u \in N$

[0082] are considered. The stored sets of data D_{jk} of the recovery boiler are consequently (n+m) tupels:

$$D_{jk} = \begin{pmatrix} x_j \\ \Phi_{jk} \end{pmatrix}, \quad k = 1, 2, ..., v_j; \quad j = 1, 2, ..., u$$
 (16).

[0083]

[0084] In this case, D_{j1k1} is stored before D_{j2k2} if

$$(j_1 < j_2) \lor ((j_1 = j_2) \land (k_1 < k_2))$$

[0086] applies.

DATA COMPRESSION BY CLASSIFICATION OF THE PARAMETERS

[0087] Since for each manipulated variable tupel x there

are generally a number of realizations of Φ_x , a classification of the parameters by forming arithmetic mean values is a suitable operation as a first step of the statistical data analysis on account of the complex stochastic properties of the process to be considered. Moreover, sets of data which are obviously erroneous are picked out. A set of data which is obviously erroneous is, for example, a physically impossible measurement which cannot occur in reality, particularly due to a setting made.

[0088] Procedure:

- 1. Sets of data in which the "BL Front Pressure" variable is not equal to the "BL Back Pressure" variable are picked out, since these two values must be equal according to the default of the plant control. The data loss is very small.
- The sets of data are divided into classes in which the four setting parameters (PA, SA, TA, BL Front Pressure, see above) are constant in temporal succession,

[0089] i.e., the jth class comprises the data sets $D_{i\bullet}$.

- Classes in which there are fewer than 30 data sets are picked out in order that transient phenomena have no great influence.
- 4. For each class, an arithmetic mean value Φ_j —and an empirical standard deviation s_j are determined for all the measured variables.

$$\overline{\Phi}_{j} = \frac{1}{v_{j}} \cdot \sum_{k=1}^{v_{j}} \Phi_{jk} \qquad (17),$$

$$s_{j} = \begin{pmatrix} \left[\frac{1}{v_{j} - 1} \cdot \sum_{k=1}^{v_{j}} \left(\Phi_{jk}^{(l)} - \overline{\Phi}_{j}^{(l)} \right)^{2} \right]^{\frac{1}{2}} \\ \vdots \\ \left[\frac{1}{v_{j} - 1} \cdot \sum_{k=1}^{v_{j}} \left(\Phi_{jk}^{(m)} - \overline{\Phi}_{j}^{(m)} \right)^{2} \right]^{\frac{1}{2}} \end{pmatrix}$$

$$(18).$$

[0090]

5. Classes in which the mean values for the variables PA, SA, TA or BL Front Pressure are too far away from the corresponding setting parameters are picked out. Therefore, in these classes it is not possible to reach the setting values.

STATISTICAL CHARACTERISTIC VARIABLES FOR THE GIVEN CLASSES AND THEIR GRAPHIC REPRESENTATION

[0091] Apart from the arithmetic mean values and the empirical standard deviations which were determined for the individual classes, a common standard deviation s is also determined according to

$$\mathbf{s} = \begin{bmatrix} \left(\frac{1}{v-1} \cdot \sum_{j=1}^{u} (v_{j} - 1) \mathbf{s}_{j}^{(1)2}\right)^{\frac{1}{2}} \\ \vdots \\ \left(\frac{1}{v-1} \cdot \sum_{j=1}^{u} (v_{j} - 1) \mathbf{s}_{j}^{(m)2}\right)^{\frac{1}{2}} \end{bmatrix}$$
(19)

[0092]

where u stands for the number of classes (here 205) and v stands for the sum of v_i , i.e., v is the number of all the measured values used (here 38915).

LINEAR REGRESSION MODELS FOR FUNCTION APPROXIMATIONS

[0094] For each measured variable (item of measurement data) $\Phi^{(i)}$ (i=1,2,...,m), a linear regression model is calculated on the basis of the arithmetic mean over the classes in dependence on the quadratic combination of the four setting parameters. In the following representation, $x \in R^4$, where

[0095] x(1): Primary Air (PA)

[0096] $x^{(2)}$: Secondary Air (SA)

[0097] $x^{(3)}$: Tertiary Air (TA)

[0098] $x^{(4)}$: Black Liquor (BL) Front Pressure

[0099] applies. $u \in N$ denotes the number of classes. Each measured variable $\Phi^{(i)}$ is modeled by

$$\Phi^{(i)}(x,\omega) = a_i^T r(x) + e_i(\omega)$$
 (20)

[00100]

[00101] with $a_i \in R^{15}$. Here the following applies:

$$r: \mathbf{R}^4 \to \mathbf{R}^{15} \tag{21}$$

$$(\zeta_{1}, \zeta_{2}, \zeta_{3}, \zeta_{4})^{T} \rightarrow (1, \zeta_{1}, \zeta_{2}, \zeta_{3}, \zeta_{4}, \zeta_{1}^{2}, \zeta_{2}^{2}, \zeta_{3}^{2}, \zeta_{4}^{2}, \zeta_{1}^{2}, \zeta_{1}^{$$

[00102]

[00103] i.e., polynomials of the second degree are adapted to the measurement data, and

$$e_i: \Omega \to \mathbb{R}$$
 (23)

[00104]

[00105] is a random variable with the expected value 0.

[00106] The vector ai is determined by the method of

[00107] least squares, but the arithmetic means

 $\left(x_{j},\Phi_{j}^{(i)}\right)$

[00109] are used instead of the original data sets

$$\left(x_{j},\,\overline{\Phi}_{j}^{(i)}\right)$$

[00110]

[00111] This procedure is suitable, since linear regression models estimate in particular expected values. This results in the following minimization problem:

$$\underset{a_{\underline{i}} \in \mathbf{R}^{15}}{\min} \left\{ \left\| \left(\overline{\phi}_{\underline{i}}^{(\underline{i})} \right) - \left(\begin{matrix} r(\mathbf{x}_{1})^{T} \\ \vdots \\ r(\mathbf{x}_{u})^{T} \end{matrix} \right) \cdot \left(\begin{matrix} a_{\underline{i}}^{(1)} \\ \vdots \\ a_{\underline{i}}^{(15)} \end{matrix} \right) \right\|_{2}^{2} \right\}$$
 (24).

[00112]

[00113] Let a_i be the optimum point of the quadratic minimization problem from equation (24). Furthermore, the following applies:

$$\hat{\mathbf{y}}_{\underline{\mathbf{i}}} := \begin{pmatrix} \mathbf{r}(\mathbf{x}_{\underline{\mathbf{1}}})^{T} \\ \vdots \\ \mathbf{r}(\mathbf{x}_{\underline{\mathbf{u}}})^{T} \end{pmatrix} \cdot \begin{pmatrix} \overline{\mathbf{a}}_{\underline{\mathbf{i}}}(\underline{\mathbf{1}}) \\ \vdots \\ \overline{\mathbf{a}}_{\underline{\mathbf{i}}}(\underline{\mathbf{1}},\underline{\mathbf{5}}) \end{pmatrix} \in \mathbf{R}^{\underline{\mathbf{u}}}$$
(25),

$$\overline{y}_{\underline{i}} := \frac{1}{u} \cdot \sum_{j=1}^{u} \overline{\Phi}_{\underline{j}}^{(\underline{i})} \in \mathbf{R}$$
(26).

[00114]

[00115] To validate the regression theorem, a coefficient of determination R^2 is calculated according to

$$R^{2} := \frac{\sum_{j=1}^{u} \left(\hat{y}_{1}^{(j)} - \overline{y}_{1}\right)^{2}}{\sum_{i=1}^{u} \left(\overline{\Phi}_{j}^{(i)} - \overline{y}_{1}\right)^{2}} = \frac{\hat{y}_{1}^{T} \hat{y}_{1} - u \overline{y}_{1}^{2}}{\overline{\Phi}^{(i)} T \overline{\Phi}^{(i)} - u \overline{y}_{1}^{2}}$$
(27)

[00116]

[00117] with

$$\overline{\Phi}^{(i)} = \begin{pmatrix} \overline{\Phi}_{1}^{(i)} \\ \vdots \\ \overline{\Phi}_{u}^{(i)} \end{pmatrix}$$
(28).

[00118]

[00119] The closer R^2_i is to 1, the better the dependent variable is represented by the independent variables $\left(0 \le R_1^2 \le 1\right)$

[00120] In addition, a maximum $E^{(i)}_{\ max}$ for an absolute value of the deviation of the data from the model is specified as

$$E_{\max}^{(i)} := \max_{j=1,\dots,1} \left\{ |\overline{\Phi}_{j}^{(i)} - \hat{y}_{i}^{(j)}| \right\}$$
 (29).

[00121]

[00122] $E^{(i)}_{90\%}$ is that value below which at least 90% of the absolute values of the deviations of the data from the model lie. By analogy with this, $E^{(i)}_{90\%}$ is that value below which at least 80% of the absolute values of the deviations of the data from the model lie. With the optimum point a_i of the minimization problem according to equation (24), a model $\tilde{\Phi}^{(i)}$ of the expected value of the measured variable $\Phi^{(i)}$ can be specified as

$$\tilde{\Phi}^{(i)} := \mathbb{R}^n \to \mathbb{R} \tag{30},$$

$$x \to \overline{a}_i^T r(x) \tag{31}.$$

[00123]

[00124] — In particular, the gradient $\nabla \widetilde{\Phi}^{(i)}$ can be analytically specified by

$$\nabla \widetilde{\Phi}^{(\underline{i})}(x) = \frac{dr}{dx}(x) \cdot \overline{a}_{\underline{i}} \quad \text{for all} \quad x \in \mathbb{R}^n$$
 (32).

[00125]

[00126] The above-described method and system are illustrative of the principles of the present invention. Numerous modifications and adaptations will be readily apparent to those skilled in this art without departing from the spirit and scope of the present invention.

ABSTRACT

[00127] A method is provided for designing a technical system in which measurement data of a predetermined system are described based on a substitute model. A numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. On the basis of the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible. The substitute model adapted with regard to its quality is used for designing the technical system.

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Description

Method and arrangement for designing a technical system

5 The invention relates to a method and arrangement for designing a technical system.

The system behavior of a technical system, for example a process engineering plant or system in heavy industry, depends on numerous parameters. In the course of designing such a system, that is in particular in the case of a new design or when adapting or adjusting an already existing system, it is necessary to comply with preconditions, for example with regard to the cost-effectiveness or environmental impact of the system. Each precondition is formulated as a target function, the optimization of which with regard to the other target functions is the general aim.

The **object** of the invention is to make it possible for a technical system to be designed on the basis of measurement data of a predetermined system. Specifically with regard to the optimization of the existing system or with regard to an optimized new design of a system, such use of known measurement data is of great significance.

This object is achieved according to the features of the independent patent claims.

Developments of the invention also emerge from the dependent claims.

To achieve the object, a method for designing a technical system in which measurement data of a predetermined system are described on the basis of a substitute model is specified. A numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. On the basis of the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible.

The substitute model adapted with regard to its quality is used for designing the technical system.

The measurement data obtained from many different realized systems are used for describing the 5 substitute model. With the substitute model it is attempted to replicate the predetermined system as well as possible. The numerical value for the quality of the replication is determined by comparing the actual measurement data with the data obtained on the basis of the substitute model. A great difference between the 10 measurement data and the data of the substitute model corresponds to poor quality, that is poor mapping of the predetermined system into the substitute model. The numerical value for the quality is used to adapt the substitute model to make the quality itself become 15 as high as possible and consequently to make the substitute model describe the predetermined system as well as possible. The high-quality substitute model obtained in this way is used for designing the 20 technical system.

Designing is understood in a general sense as meaning both the new design of a technical system and the adaptation of an already existing technical system.

One development comprises that the substitute 25 model is a regression model. The regression model is based on the description

$$Y_i = f_\beta(x_i) + e_i$$

where

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 (y_i, x_i) denotes predetermined pairs of values,

 f_{β} denotes a function which is dependent on a parameter $\beta,$ and

e: denotes an error.

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It is then intended to minimize the error (as a function of $\beta):$

$$\sum_{i=1}^{n} e_i^2 = \varphi(\beta).$$

If the following example

 $Y = \beta_0 + \beta_1 x + \beta_2 x^2 + e$

is taken as a basis, the functional relationship is of a quadratic order, while the regression model (function, dependent on $\beta)$ is linear.

In another development, the quality can be determined on the basis of a mean square deviation of the measurement data from the data determined by the substitute model. The adaptation of the substitute model takes place by minimizing the mean square deviation.

One refinement comprises that the measurement data are sorted according to their quality, with respect to the deviation of the latter from the data determined by the substitute model, and a predetermined number of n% of the worst measurement data are picked out. Consequently, a quality is determined for each item of measurement data, the volume of measurement data, preferably in the form of a list, being sorted according to their quality and the n% of the worst measurement data, or the n worst measurement data, being picked out. In particular, it must be checked whether the n% of worst measurement data or n worst measurement data lie in a continuous range. If this is the case, these measurement data are not picked out, since they very probably do not represent measurement errors but a continuous range which is not mapped accurately enough by the substitute model.

Another development comrises that the measurement data are subjected to a preprocessing operation. Since, in an actual predetermined system, a large amount of measurement data occur per

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unit of time, it is advisable to subject these measurement data to a preprocessing operation and that largely consequently ensure significant measurement data are taken for forming the substitute The preprocessing operation preferably finds its expression in a reduction in the number of measurement data.

In the process, the measurement data are divided into classes according to predetermined criteria. The measured values of a class are assessed and those measured values for which the assessment lies below a predetermined first threshold value are picked out. The picking out of the measured values results in a reduction with regard to the number of measured values. This results in a significantly reduced number of measured values for a further processing operation. The further processing operation can take place with less computing effort in comparison with the unreduced number of measured values.

The classes themselves can also be assessed. In particular, a class for which the assessment lies below a predetermined second threshold value can be picked out. As a result, an additional reduction of the number of measured values is obtained.

Another development of the preprocessing comprises that a criterion for classification is that, for each class, measured values are determined as a default for setting parameters of the technical system. The technical system is typically set on the basis of a predetermined number of setting parameters; after setting, a reaction of the system to the setting parameters takes place (usually with a time delay) (transient response, transient phenomenon of the system). After setting, consequently 3.5 a certain set of measured values which can be assigned to the transient phenomenon are recorded, with measured values continuing to occur after the transient phenomenon has come to an end (transition to steadystate operation), and

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are assigned to the predetermined set of setting parameters. By adjusting the setting parameters, a new class is determined. All the measured values which respectively occur after adjustment of the setting parameters belong in a class of their own.

In addition, measured values of a class which can be assigned to the respective transient phenomenon can be picked out. Furthermore, erroneous measured values can be picked out. The setting of large technical systems is in many cases directed at longterm steady-state operation. It is advisable for the values which relate to the transient measured phenomenon (of short duration in relation to the steady-state operation after the transient phenomenon 15 has come to an end) to be picked out, since they have the effect of falsifying measured values for steadystate operation. In particular when modeling the technical system, the measurement data of the steadystate behavior of the system are of interest.

One refinement comprises reducing the number of measured values in a class by determining at least one representative value for the measured values of the class. Such a representative value may be:

- a) a mean value (for example a sliding mean value) of the measured values of the class,
- b) a maximum value of the measured values of the class.
- a minimum value of the measured values of the class,
- a median. d)

In the case of variant d), one advantage is that a value which actually exists can always be determined, whereas the mean value a) does not itself occur as a value.

35 Depending on the application, a suitable choice can be made for determining the representative value of a class.

An entire class with measured values may be picked out if it contains less than a predetermined number of measured values.

Another refinement comprises that those

5 measured values which vary by more than a predetermined
threshold value from a predeterminable value are picked
out. The predeterminable value may be a mean value of
all the measured values of the class or a measured
value to be expected in response to the respective

10 setting parameters of the technical system.

Within another development, the data obtained by means of designing are used for controlling a technical plant. In addition, the controlling of the technical plant can take place at the running time of the system, that is online.

Also specified for achieving the object is an arrangement for designing a technical system which has a processor unit, which processor unit is set up in such a way that measurement data of a predetermined 20 system can be described on the basis of a substitute model. A numerical value for the quality of the substitute model can be determined by comparing the measurement data of the predetermined system with data determined by the substitute model. On the basis of the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible. The substitute model adapted with regard to its quality is used for designing the technical system.

This arrangement is particularly suitable for carrying out the method according to the invention or one of its developments explained above.

Exemplary embodiments of the invention are presented and explained below with reference to the drawing,

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in which:

figure 1 shows a block diagram which contains steps of a method for designing a technical system; figure 2 shows a schematic diagram of a

recovery boiler;

figures 3-5 show input variables, manipulated variables and output variables of the recovery boiler.

Represented in figure 1 is a block diagram which contains steps of a method for designing a technical system. In a step 101, a substitute model is formed on the basis of measurement data. substitute model is preferably a regression model. adapt the substitute model created in step 101 to the measurement data, that is to perform a refinement of the substitute model, so that the measurement data substitute model describe the in adequate approximation, a numerical value for the quality of the substitute model is determined in a step 102. numerical value is determined by comparing 20 measurement data of the predetermined system with data determined by the substitute model. Each item of measurement data preferably receives a numerical value for the quality, which numerical value characterizes the deviation of the item of measurement data from the associated value determined by the substitute model. The sum of all the numerical values for the quality for all the measurement data determines an overall quality for the substitute model. In a step 103, the quality is maximized by minimizing the numerical value for the quality (or a negative quality for the coincidence of the substitute model with the predetermined system). Once an appropriately high quality for the substitute model has been determined, this substitute model is used for designing the technical system in a step 104. The designing may constitute both a new design (cf. step 105) or an adaptation of an already existing

35 technical system (cf. step 106).

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Figure 2 shows a schematic diagram of a recovery boiler. An exemplary embodiment of the method described above is illustrated below on the basis of the example of a "recovery boiler".

In the paper and pulp industry, various chemicals and also heat and electrical energy are required for the digestion of pulp. The recovery boiler can be used to recover the chemicals used and also thermal energy from a concentrated process liquor (black liquor). A measure of the recovery of the chemicals is of decisive significance for the costeffectiveness of the overall plant.

The black liquor is combusted in a char bed 201. As this happens, an alkali fusion is formed, 15 flowing away via a line 202. In further process steps, the chemicals used are recovered from the constituents of the alkali fusion. Released heat of combustion is used for generating steam. The combustion of the waste liquor and consequently the recovery of the chemicals 20 begins with the atomization of the black liquor via atomizer nozzles 204 into a combustion chamber 203. Particles of the atomized black liquor are dried as they fall through the hot flue gas. The dried liquor particles fall onto the char bed 201, with a first combustion and a chemical reduction taking place. Volatile constituents and reaction products pass into an oxidation zone, in which oxidizing reactions proceed and in which the combustion is completed.

Important targets for the controlling of the recovery boiler are the steam production for obtaining 30 energy, the maintaining of emission values from environmental aspects and the efficiency of the chemical reduction.

The combustion operation, and consequently the targets, are controlled in particular by the air supply on three levels (Primary Air (PA), Secondary Air (SA), Tertiary Air (TA)). The overall process is subject to numerous influences, which have to be taken into account in the modeling:

- a) the measurement of the variables is often subject to strong fluctuations;
- b) unmeasured and unmeasurable influencing variables exist;
 - any alteration of the parameters which can be set causes transient phenomena;
 - d) the technical plant becomes soiled and is cleaned at predetermined intervals, having the result each time of a temporal drift in the system behavior.

The measured variables of the overall process 20 are divided into input variables (cf. figure 3) and output variables (cf. figure 5). Measured values are stored every minute. Four of the input variables are at the same time also manipulated variables (also: parameters which can be set; cf. figure 4). manipulated variables are to be regarded essentially as 25 free parameters of the overall process which can be set independently of one another. Some of the other input variables are more or less dependent on the manipulated variables. According to one target, in the case of the recovery boiler the "BL Front Pressure" and "BL Back Pressure" variables are always to be controlled such that they are the same. The four manipulated variables (cf. figure 4) are preferably to be manipulated variables (with the desired, preset value) 35 and as input variables (with the measured, actual value).

In the case of the recovery boiler, one problem is that of meeting targets which are determined in dependence on the parameters to be set and

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are defined by means of measured variables. A three-stage procedure is chosen here to solve the problem:

- 1. The targets to be considered are modeled by stochastic methods, these models being updated by new measurements (data-driven, empirical modeling). For this it is advisable to use not just a single model but instead global models for the identification of areas of interest in a parameter space determined by the targets and local models for the exact calculation of optimum operating points. The models used are assessed by measures of quality.
- 2. If the models considered are not sufficiently
 accurate (measure of quality) on account of the data
 situation, new operating points are evaluated on a
 specific basis to improve the model (experimental
 design). Furthermore, by the use of global
 stochastic optimizing methods with respect to the
 targets, attractive areas are identified in
 dependence on the current global model.
 - For the local optimization, local models are devised and, if appropriate, the available sets of data are extended on a specific basis (experimental design).

The targets constitute physical-technical or business-management criteria, which generally have to conform to boundary conditions and/or safety conditions. Often a number of these criteria have to be considered simultaneously. The use of a stochastic model can be used in particular to simulate in the computer the target variables to be optimized and their dependence on the parameters to be set. This is necessary whenever measurements are very cost-intensive

or very time-consuming. In the case of safety requirements, possible hazardous situations can be avoided.

In the case of the recovery boiler, an online optimization which is based on a number of data is necessary because the physical-chemical processes cannot be quantitatively modeled with sufficient accuracy and because the behavior of the plant is subject to fluctuations in the course of operation. Knowledge of this behavior must be continually extended by selective choice of new operating points. Therefore, the already described three-stage procedure of stochastic modeling and mathematical optimization is recommendable as part of online optimization.

DESCRIPTION OF THE INPUT VARIABLES

The a input variables (a \in N, N: set of natural numbers) are generally dependent on n actuated variables n \in N and on random effects. They can be described as follows:

Let (Ω, S, P) be a probability space and B^v be a Borel σ algebra over P' (P: set of real numbers) for each $v \in N$. The input variables are represented by means of a $B^n \times S - B^n$ -measurable mapping ϕ :

$$\varphi: \mathbf{R}^{\mathbf{n}} \times \Omega \to \mathbf{R}^{\mathbf{a}} \tag{1}.$$

The domain of the mapping ϕ is a Cartesian product of two sets. If the respective projections onto the individual sets are considered, the following mappings are obtained:

$$\phi_{\mathbf{X}}: \Omega \to \mathbb{R}^{\mathsf{a}}, \ \omega \to \phi(\mathbf{x}, \omega) \quad \text{ for all } \mathbf{x} \in \mathbb{R}^{\mathsf{D}}$$
 (2),

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$$\varphi^{\omega} \colon R^{n} \to R^{a}, \ x \to \varphi(x, \omega) \quad \text{for all } \omega \in \Omega$$
 (3).

 $\begin{cases} \phi_X, \ x \in R^n \end{cases} \quad \text{is a stochastic process with an index set} \\ \bigwedge^R, \quad \text{and a mapping } \phi^\omega \text{ is, for each event } \omega \in \Omega,$ a path of this stochastic process.}

In the case of the recovery boiler, n=4 and a=14 (after elimination of the "BL Back Pressure" variable).

On account of the required measurability of the mapping ϕ_x , for each $x \in X^{a^n}$ the mapping ϕ_x is a random variable. Under suitable additional preconditions, expectation values and higher moments can be considered. This approach permits the step from stochastic models to deterministic optimization problems. In the case of a deterministic optimization problem, the target function can be set directly by means of a variable, whereas the stochastic variable influences the target function but does not permit a specific setting.

20 DESCRIPTION OF THE OUTPUT VARIABLES

The process model M of the recovery boiler is described as a function in dependence on the input variables and further random effects. In this case let (Ω, S, P) be the above probability space. The process model M is then a $\mathbf{B}^a \times \mathbf{S} - \mathbf{B}^b$ -measurable mapping:

$$M: \mathbf{R}^{\mathbf{a}} \times \Omega \to \mathbf{R}^{\mathbf{b}} \tag{4}$$

30 where b denotes the number of output variables.

Since the recovery boiler is subject to a cyclical temporal drift (from cleaning phase to

cleaning phase), a description with a time parameter is also conceivable. The

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output variables can be represented by B^{n} \times S - $B^{\text{b}}\text{-}$ measurable mappings $\psi\colon$

$$\Psi: \mathbf{R}^{\mathbf{n}} \times \Omega \to \mathbf{R}^{\mathbf{b}} \tag{5}$$

$$(x, \omega) \to M(\phi(x, \omega), \omega)$$
 (6).

If the respective projections onto the individual sets of the domain are considered, the following mappings are obtained

$$\psi_{\mathbf{X}} \colon \Omega \to \mathbb{R}^{\mathbf{b}}, \ \omega \to \psi(\mathbf{x}, \omega) \quad \text{for all} \quad \mathbf{x} \in \mathbb{R}^{\mathbf{n}}$$
 (7),

$$\psi^{\omega} \colon \mathbb{R}^{n} \to \mathbb{R}^{b}, \ x \to \psi(x, \omega) \text{ for all } \omega \in \Omega$$
 (8).

 $\left\{ \psi_X; \ x \in R^n \right\} \text{ is a stochastic process with an index set } \tilde{R}^n, \text{ and the mapping } \psi^n \text{ is, for each } \omega \in \Omega, \text{ a path of this stochastic process.}$

In the case of the recovery boiler, b=15.

The fact that in the definition of ψ a distinction is not drawn between the events ω used does not mean that there is any restriction, since Ω can be represented as a Cartesian product of an Ω_1 and an Ω_2 . The above representation consequently also comprises the model:

$$\Psi: \mathbf{R}^{n} \times \Omega_{1} \times \Omega_{2} \to \mathbf{R}^{b} \tag{9}$$

$$(x, \omega_1, \omega_2) \rightarrow M(\varphi(x, \omega_1), \omega_2)$$
 (10).

DESCRIPTION OF THE AVAILABLE SETS OF DATA

With the descriptions in the two foregoing sections, the input variables and the output variables can be combined together to form measured variables (= measurement data) Φ . Φ is a $B^n \times S$ - B^n -measurable measurable with m = a + b and

$$\Phi: \mathbf{R}^{n} \times \Omega \to \mathbf{R}^{m} \tag{11}$$

$$(x, \omega) \rightarrow \begin{pmatrix} \varphi(x, \omega) \\ \psi(x, \omega) \end{pmatrix}$$
 (12).

If the respective projections onto the individual sets of the domain are again considered, the 10 following mappings are obtained:

$$\Phi_X: \Omega \to \mathbb{R}^m, \ \omega \to \Phi(x, \omega) \quad \text{for all} \quad x \in \mathbb{R}^n$$
 (13),

$$\Phi^{\omega} \colon \mathbb{R}^{n} \to \mathbb{R}^{m}, \ x \to \Phi(x, \omega) \quad \text{for all} \quad \omega \in \Omega$$
 (14).

 $\left\{ \Phi_{x},\;x\in\mathbf{R}^{n}\right\} \quad\text{is a stochastic process with an index set}\\ X^{n},\;\text{and the mapping }\Phi^{n}\;\text{is, for each }\omega\in\Omega,\;\text{a path of}\\ \text{this stochastic process.}$

For each chosen related variable tupel x, in the case of the recovery boiler many realizations of Φ_x are determined and stored, i.e. for each $x_3 \in \mathbb{N}^n$ numerous realizations

$$\Phi_{jk} := \Phi(x_j, \omega_{jk}) \tag{15}$$

with $\omega_{jk} \in \Omega$; $k = 1,2,...,v_j$;

$$v_j \in N$$
; $j = 1,2,...,u$; $u \in N$

are considered. The stored sets of data D_{jk} of the recovery boiler are consequently (n+m) tupels:

$$D_{jk} = \begin{pmatrix} x_j \\ \Phi_{jk} \end{pmatrix}, \qquad k = 1,2,\dots,v_j; \quad j = 1,2,\dots,u \tag{16} \ .$$

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In this case, D_{31k1} is stored before D_{32k2} if
$$(j_1 < j_2) \vee ((j_1 = j_2) \wedge (k_1 < k_2))$$
 applies.

10 DATA COMPRESSION BY CLASSIFICATION OF THE PARAMETERS

Since for each manipulated variable tupel x there are generally a number of realizations of Φ_{xx} , a classification of the parameters by forming arithmetic 15 mean values is a suitable operation as a first step of the statistical data analysis on account of the complex stochastic properties of the process to be considered. Moreover, sets of data which are obviously erroneous are picked out. A set of data which is obviously 20 erroneous is, for example, a physically impossible measurement which cannot occur in reality, in particular on account of a setting made.

Procedure:

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- 1. Sets of data in which the "BL Front Pressure" variable is not equal to the "BL Back Pressure" variable are picked out, since these two values must be equal according to the default of the plant control. The data loss is very small.
- The sets of data are divided into classes in which the four setting parameters (PA, SA, TA, BL Front Pressure, see above) are constant in temporal succession.

i.e. the jth class comprises the data sets Di.

- Classes in which there are fewer than 30 data sets are picked out in order that transient phenomena have no great influence.
- 4. For each class, an arithmetic mean value $\overline{\Phi}_j$ and an empirical standard deviation s_j are determined for all the measured variables:

$$\overline{\Phi}_{j} = \frac{1}{v_{j}} \cdot \sum_{k=1}^{v_{j}} \Phi_{jk} \qquad (17),$$

$$s_{j} = \begin{pmatrix} \left[\frac{1}{v_{j}-1} \cdot \sum_{k=1}^{v_{j}} \left(\Phi_{jk}^{(l)} - \overline{\Phi}_{j}^{(l)}\right)^{2}\right]^{\frac{1}{2}} \\ \vdots \\ \left[\left(\frac{1}{v_{j}-1} \cdot \sum_{k=1}^{v_{j}} \left(\Phi_{jk}^{(m)} - \overline{\Phi}_{j}^{(m)}\right)^{2}\right]^{\frac{1}{2}} \end{pmatrix} \end{cases}$$

$$(18).$$

5. Classes in which the mean values for the variables PA, SA, TA or BL Front Pressure are too far away from the corresponding setting parameters are picked out. Therefore, in these classes it was not possible to reach the setting values.

STATISTICAL CHARACTERISTIC VARIABLES FOR THE GIVEN CLASSES AND THEIR GRAPHIC REPRESENTATION

Apart from the arithmetic mean values and the sempirical standard deviations which were determined for the individual classes, a common standard deviation s is also determined according to

$$s = \begin{pmatrix} \left(\frac{1}{v-1} \cdot \sum_{j=1}^{u} (v_{j} - 1) s_{j}^{(1)2}\right)^{\frac{1}{2}} \\ \vdots \\ \left(\frac{1}{v-1} \cdot \sum_{j=1}^{u} (v_{j} - 1) s_{j}^{(m)2}\right)^{\frac{1}{2}} \end{pmatrix}$$
(19)

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where u stands for the number of classes (here 205) and v stands for the sum of $v_{\rm j}$, i.e. v is the number of all the measured values used (here 38915).

15 LINEAR REGRESSION MODELS FOR FUNCTION APPROXIMATIONS

For each measured variable (item of measurement data) $\Phi^{(i)}$ (i=1,2,...,m), a linear regression model is calculated on the basis of the arithmetic mean over the classes in dependence on the quadratic combination of the four setting parameters. In the following representation, $x \in \mathbb{R}^4$, where

x(1): Primary Air (PA)

x(2): Secondary Air (SA)

x(3): Tertiary Air (TA)

x(4): Black Liquor (BL) Front Pressure

applies. u \in N denotes the number of classes. Each measured variable $\Phi^{(i)}$ is modeled by

$$\Phi^{(i)}(x,\omega) = a_i^T r(x) + e_i(\omega)$$
 (20)

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with $a_{i}\,\in\,\boldsymbol{R}^{15}.$ Here the following applies:

$$r: \mathbf{R}^4 \to \mathbf{R}^{15} \tag{21}$$

$$(\zeta_1, \zeta_2, \zeta_3, \zeta_4)^T \rightarrow (1, \zeta_1, \zeta_2, \zeta_3, \zeta_4, \zeta_1^2, \zeta_2^2, \zeta_3^2, \zeta_4^2, \zeta_4^2, \zeta_5^2, \zeta_5^2,$$

i.e. polynomials of the second degree are adapted to the measurement data, and

$$e_i: \Omega \to R$$
 (23)

is a random variable with the expected value 0.

The vector a_i is determined by the method of least squares, but the arithmetic means $\left(x_{\dot{\gamma}}, \, \Phi_{\dot{\gamma}\,\dot{k}}^{(i)}\right)^T$

are used instead of the original data sets

$$\left(x_{j}, \overline{\Phi}_{j}^{(i)}\right)^{T}$$

This procedure is suitable, since linear regression models estimate in particular expected values. This results in the following minimization problem:

$$\min_{\substack{\mathbf{a}_{\dot{1}} \in \mathbf{R}^{15}}} \left\{ \left\| \begin{pmatrix} \overline{\Phi}_{\dot{1}}^{(i)} \\ \vdots \\ \overline{\Phi}_{\dot{u}}^{(i)} \end{pmatrix} - \begin{pmatrix} \mathbf{r}(\mathbf{x}_{\dot{1}})^T \\ \vdots \\ \mathbf{r}(\mathbf{x}_{\dot{u}})^T \end{pmatrix} \cdot \begin{pmatrix} \mathbf{a}_{\dot{1}}^{(1)} \\ \vdots \\ \mathbf{a}_{\dot{1}}^{(15)} \end{pmatrix} \right\|_{2}^{2} \right\}$$
 (24).

Let $\overline{a_i}$ be the optimum point of the quadratic minimization problem from equation (24). Furthermore, the following applies:

$$\hat{\mathbf{y}}_{\underline{\mathbf{i}}} := \begin{pmatrix} \mathbf{r}(\mathbf{x}_{1})^{T} \\ \vdots \\ \mathbf{r}(\mathbf{x}_{u})^{T} \end{pmatrix} \cdot \begin{pmatrix} \mathbf{\bar{a}}_{\underline{\mathbf{i}}}^{(1)} \\ \vdots \\ \mathbf{\bar{a}}_{\underline{\mathbf{i}}}^{(1.5)} \end{pmatrix} \in \mathbf{R}^{\mathbf{u}}$$
(25),

$$\overline{y}_{i} := \frac{1}{u} \cdot \sum_{j=1}^{u} \overline{\Phi}_{j}^{(i)} \in \mathbf{R}$$

$$(26).$$

To validate the regression theorem, a coefficient of determination $\ensuremath{R^2}$ is calculated according to

$$\mathbf{R}^{2} := \frac{\sum_{j=1}^{u} \left(\hat{\mathbf{y}}_{1}^{(j)} - \overline{\mathbf{y}}_{1}\right)^{2}}{\sum_{j=1}^{u} \left(\overline{\mathbf{\Phi}}_{j}^{(i)} - \overline{\mathbf{y}}_{1}\right)^{2}} = \frac{\hat{\mathbf{y}}_{1}^{T} \hat{\mathbf{y}}_{1} - u \overline{\mathbf{y}}_{1}^{2}}{\overline{\mathbf{\Phi}}^{(i)T} \overline{\mathbf{\Phi}}^{(i)} - u \overline{\mathbf{y}}_{1}^{2}}$$
(27)

wit t

$$\overline{\Phi}^{(i)} = \begin{pmatrix} \overline{\Phi}_{1}^{(i)} \\ \vdots \\ \overline{\Phi}_{u}^{(i)} \end{pmatrix} \tag{28}.$$

The closer R^2 ₁ is to 1, the better the dependent variable is represented by the independent variables 15 $\left(0 \le R_1^2 \le 1\right)$

In addition, a maximum $E^{(i)}_{\text{max}}$ for an absolute value of the deviation of the data from the model is specified as

$$E_{\text{max}}^{(i)} := \max_{j=1,\dots,u} \left\{ \overline{\Phi}_{j}^{(i)} - \hat{y}_{i}^{(j)} \right\}$$
(29).

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 $E^{(i)}_{90\%}$ is that value below which at least 90% of the absolute values of the deviations of the data from the model lie. By analogy with this, $E^{(i)}_{80\%}$ is that value below which at least 80% of the absolute values of the deviations of the data from the model lie. With the optimum point $\overline{a_i}$ of the minimization problem according to equation (24), a model $\tilde{\Phi}^{(i)}$ of the expected value of the measured variable $\Phi^{(i)}$ can be specified as

$$\tilde{\Phi}^{(i)} := \mathbb{R}^n \to \mathbb{R} \tag{30},$$

$$x \to \overline{a}_{\underline{i}}^{T} r(x) \tag{31}.$$

In particular, the gradient $\nabla\widetilde{\Phi}^{(i)}$ can be analytically specified by

$$\nabla \widetilde{\Phi}^{\left(\underline{i}\right)}(x) = \frac{dr}{dx}(x) \cdot \overline{a}_{\underline{i}} \quad \text{for all} \quad x \in \mathbf{R}^{n} \tag{32} \ .$$

Patent claims

- 1. A method for designing a technical system,
- 5 a) in which measurement data of a predetermined system are described on the basis of a substitute model;
- b) in which a numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model;
- c) in which the substitute model is adapted from the numerical value for the quality to be of as high a quality as possible;
- d) in which the substitute model adapted with 20 regard to its quality is used for designing the technical system.
 - 2. The method as claimed in claim 1, in which the substitute model is a regression model.
- 25 3. The method as claimed in claim 1 or 2, in which the quality is determined on the basis of a mean square deviation of the measurement data from the data determined by the substitute model.
- 4. The method as claimed in one of the preceding 30 claims, in which the measurement data are sorted according to their quality, with respect to the deviation of the latter from the data determined by the substitute model, and a predetermined number of n% of the worst measurement data are picked out.
- 35 5. The method as claimed in claim 4, in which the n\$ of the worst measurement data are not picked out

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if they lie in a continuous range.

- 6. The method as claimed in one of the preceding claims, in which the amount of measurement data is reduced in the course of a preprocessing operation.
- 5 7. The method as claimed in claim 6, in which the preprocessing operation comprises a classification of the measurement data.
 - 8. The method as claimed in one of the preceding claims, in which the data obtained by means of designing are used for controlling a technical plant.
- The method as claimed in claim 8, for the online adaptation of the control for the technical plant.
- 10. An arrangement for designing a technical system, with a processor unit which is set up in such a way that
 - a) measurement data of a predetermined system are described on the basis of a substitute model;
 - a numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model;
 - c) the substitute model is adapted from the numerical value for the quality to be of as high a quality as possible;
 - d) the substitute model adapted with regard to its quality is used for designing the technical system.

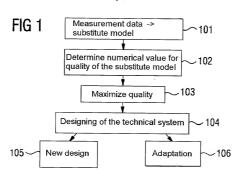
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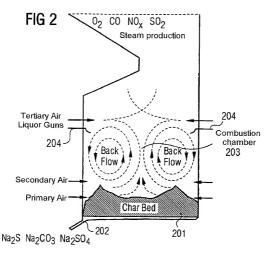
Abstract

Method and arrangement for designing a technical system

To achieve the object, a method for designing a technical system in which measurement data of a predetermined system are described on the basis of a substitute model is specified. A numerical value for the quality of the substitute model is determined by comparing the measurement data of the predetermined system with data determined by the substitute model. On the basis of the numerical value for the quality, the substitute model is adapted to be of as high a quality as possible. The substitute model adapted with regard to its quality is used for designing the technical system.







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FIG 3

Input variables		
	Measured variable Description	
1	FI 7081	BL Flow
2	QI 7082 A	Dry Solids Content
3	FIC 7280 X	PA Primary Air
4	FIC 7281 X	SA Secondary Air
5	FIC 7282 X	TA Tertiary Air
6	PI 7283	PA Pressure
7	PI 7284	SA Pressure
8	PHI 7285	TA Pressure
9	TIC 7288 X	PA Temperature
10	TIC 7289 X	SA Temperature
11	PIC 7305 X	Press Induced Draft
12	HO 7338	Oil Valve
13	TI 7347	BL Temperature
14	PIC 7349 X	BL Front Pressure
15	PIC 7351 X	BL Back Pressure

FIG 4

	Manipulated variables			
Measured variable		Description		
1	FIC 7280 X	PA Primary Air		
2	FIC 7281 X	SA Secondary Air		
3	FIC 7282 X	TA Tertiary Air		
4	PIC 7349 X	BL Front Pressure		

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FIG 5

	Outpu	t variab <u>l</u> es	
	Measured variable Description		
1	TIC 7249 X	Steam Temperature	
2	FI 7250	Steam Production	
3	QI 7322	02	
4	TI 7323	Smoke Temperature	
5	QI 7331	H ₂ S	
6	QI 7332	SO ₂	
7	QIC 7333 X	CO	
8	QIC 7370 X	Spec. Weight of Green Liquor	
9	QI 7531	NO	
10	IBM 8096	Reduction Efficiency	
11	IBM 8109	PH Value	
12	TI 7352	Bed Temperature	
13	IBM 8015	Na OH	
14	IBM 8016	Na ₂ S	
15	IBM 8017	Na 2 CO 3	

Declaration and Power of Attorney For Patent Application Erklärung Für Patentanmeldungen Mit Vollmacht German Language Declaration

	· · · · · · · · · · · · · · · · · · ·
Als nachstehend benannter Erfinder erkläre ich hiermit an Eides Statt:	As a below named inventor, I hereby declare that
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Verfahren und Anordnung zum Entwurf eines technischen Systems	
deren Beschreibung	the specification of which
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am als PCT internationale Anmeldung	was filed on as
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198 55 873.2 (Number) (Nummer)	Germany (Country) (Land)	(Day Month	mber 1998 Year Filed) Jahr eingereicht)	Yes Ja	No Nein
(Number) (Nummer)	(Country) (Land)	(Day Month (Tag Monat	Year Filed) Jahr eingereicht)	Yes Ja	No Nein
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